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10       **AN ADAPTABLE VIBRATION ABSORBER EMPLOYING A  
MAGNETORHEOLOGICAL ELASTOMER WITH VARIABLE GAP  
LENGTH AND METHODS AND SYSTEMS THEREFOR**

**Related Application**

15       This application claims priority to and the benefit of the prior filed co-  
pending and commonly owned patent application, assigned United States  
Patent Application Serial No. 60/442,241, entitled "*Tunable Adaptive  
Vibration Absorber Employing Magnetics with Variable Gap Length*", filed  
on January 24th, 2003, and incorporated herein by reference.

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**Field of the Inventions**

The inventions relate to vibration absorbers, and more particularly, the  
inventions relate to adaptive vibration absorbers including methods and  
systems related thereto.

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**Background**

A vibration absorber generally is a device used to reduce vibration in  
a structure whose motion is undesirable or whose motion is sought to be  
minimized. Vibration absorbers are commonly used in vehicles, aircraft,  
30 and other mechanisms that carry passengers – at least to provide the  
passengers with a more comfortable ride as well as for other reasons.

5           A type of vibration absorber referred to as a tuned vibration absorber  
(TVA) is used in many applications for the suppression of a specific  
vibration frequency. TVAs are used in many applications because of their  
relative low cost and well-established vibration absorption capabilities.  
TVAs, however, suffer the drawbacks of being passive devices and of being  
10   effective only for a relatively narrow bandwidth.

          Another type of vibration absorber is the active vibration controller  
(AVC). An AVC typically includes real-time property-changing  
characteristics and therefore can be highly effective. But uses of AVCs as  
vibration control mechanisms have been limited because AVCs have been  
15   costly to implement. Another problem that may arise in the use of AVC is  
that of an AVC adding energy to the system (and possibly driving the system  
into instability) in the event of an unanticipated excitation or improper  
control of the AVC.

          Thus, there is a need for a vibration absorber that includes the  
20   advantages, but does not suffer the drawbacks of the TVAs nor the  
limitations of the AVCs. There is a need for a vibration absorber that  
effectively and essentially eliminates vibration in structures and that is  
available at low cost with well-established vibration absorption capabilities.  
There is a need for a vibration absorber that may adaptively operate over a  
25   frequency range without the problems associated with adding energy to the  
system. Further, there is a need for a vibration absorber that is lightweight  
and compact.

5   **Summary**

          Stated generally, the inventions include an adaptive vibration absorber (AVA), and methods and systems therefore. Advantageously, the inventions provide an AVA that may effectively and essentially eliminate vibration in structures. The inventions provide an AVA that may operate adaptively  
10   over an appropriate relatively wide bandwidth or frequency range without adding energy to the system and the problems associated with such energy addition. Further, the inventions provide an AVA that may be of low cost as well as lightweight and compact.

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5    **Brief Description of the Drawings**

FIG. 1 is a block diagram illustrating by function an exemplary embodiment of the inventions in use with a vibrating device.

FIG. 2 is a drawing of an exemplary embodiment of the inventions.

10    FIG. 3 is a drawing of another exemplary embodiment of the inventions.

FIG. 4 is a drawing of another exemplary embodiment of the inventions.

FIG. 5 is a drawing of another exemplary embodiment of the inventions.

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## 5    **Detailed Description**

Several exemplary embodiments of the invention are described below in detail. The disclosed embodiments are intended to be illustrative only since numerous modifications and variations therein will be apparent to those of ordinary skill in the art. In reference to the drawings, like numbers  
10    indicate like parts continuously throughout the views. As utilized in the description herein and throughout the claims that follow, the meaning of “a,” “an,” and “the” include plural references also, unless the context of use clearly dictates otherwise. Additionally, the meaning of “in” includes “in” and “on” unless the context clearly dictates otherwise as the term is utilized  
15    in the description herein and throughout the claims that follow.

Generally stated, the inventions include adaptive vibration absorbers (AVAs) and methods and systems therefor. An AVA of the inventions may be considered a hybrid between a tuned vibration absorber (TVA) and an active vibration controller (AVC). The AVA includes the “active”  
20    characteristics of the AVC in that the AVA may be caused to operate selectively over a range of frequencies rather than a single frequency. One or more elements of the AVA is able to almost instantaneously and discretely change properties, thus increasing the effective bandwidth of vibration suppression by the AVA. The AVA operates like a TVA when the  
25    AVA has been set (via control algorithm or otherwise) to operate at a certain frequency.

Advantageously, the hybrid nature of the AVA may make it superior to the AVC and the TVA. The AVA may be considered to be superior to an AVC because the AVA allows switching in frequency absorption to occur  
30    only at discrete times and to discrete states. Thus, the risk of adding energy

5 to a system is virtually eliminated because the AVA behaves like a TVA between switches. The AVA may be considered superior to a TVA because the TVA may operate at more than one frequency.

The ability of the AVA of the inventions to operative selectively over a range of frequencies is brought about, in part, by the lack of geometric  
10 restraints on the AVA, and particularly, with regard to the lack of geometric constraints on certain elements of the AVA as explained below. These elements may change properties thereby increasing the bandwidth of vibration suppression by the AVA. Rather than geometric boundary conditions, the AVA may operate through the principles of force balance  
15 with respect to its elements to achieve its advantages.

Figure 1 is a block diagram that is used to illustrate the functions of an exemplary embodiment of an AVA 10 of the inventions as used with a vibrating device 12. The blocks illustrated in Figure 1 correspond to functions of the involved elements and devices. The blocks are not to be  
20 interpreted as relative sizes of the elements or devices. In fact, reference to the other figures of this patent application demonstrates that the elements of the exemplary AVA 10 may vary in size, shape, and other characteristics.

The exemplary AVA 10 is configured of the elements including a base mass 14 and an absorber mass 16 connected by a pair of switching  
25 elements 18, 20 that function effectively as tunable springs and may be held responsible for the advantageous bandwidth increase in vibration suppression by the AVA 10.

The configuration and composition of the elements 14, 16, 18 and 20 of the exemplary AVA 10 provide a path (also referred to as magnetic  
30 circuit) for magnetic flux that may be induced by a magnetic field source 22

5 connected to, disposed on or around, or located close to the exemplary AVA  
10. Specifically, the magnetic circuit through the elements of the AVA 10  
may originate with the magnetic field source 22 and pass through the  
absorber mass 16, to one of the pair of switching elements 18 (referred to as  
switching element A or S.E. A), to the base mass 14, to the other of the pair  
10 of switching elements 20 (referred to as switching element B or S.E. B), and  
so on.

The switching elements 18, 20 of the exemplary AVA are oriented in  
such a way that their static deflection lengths are determined by a force  
balance rather than geometric boundary conditions. When the source 22  
15 provides the magnetic field and flux travels through the described magnetic  
circuit, the static deflection length in each of the pair of the switching  
elements 18, 20 changes based on force balances and allowed at least in part  
because there are no geometric constraints on the elements 18, 20. Because  
the static deflection length is determined by a force balance, an increase in  
20 the magnetic attractive force causes the static deflection lengths of the  
switching elements 18, 20 to decrease and achieves a larger natural  
frequency shift than the same system limited by geometric boundary  
conditions. In this manner, a change in the applied magnetic flux may be  
used to change the frequency of vibration absorption by the AVA 10. This  
25 change may be controlled as necessary or desired via a control algorithm  
applied through a processor (not illustrated) or otherwise.

As noted, Figure 1 illustrates the functional configuration of the  
elements of the exemplary AVA 10 of the inventions. A description of  
exemplary compositions of the elements of the exemplary AVA 10 is now  
30 provided.

5           The exemplary AVA 10 includes a base mass 14 that may serve as an attachment point to the vibrating device 12. The exemplary AVA 10 may be hung in tension from the vibrating device 12 such as being hung from the vibrating device 12 by attachment to the base mass 14 of the AVA 10.

10           The base mass 14 as well as the absorber mass 16 in the exemplary embodiment are of made of relatively rigid, magnetically-conducting material such as iron or low carbon steel. One of the masses 14, 16 may be a permanent magnet. The masses 14, 16 may be of any appropriate shape such as the rectangular shapes illustrated in Figure 1, the half circle shapes illustrated in Figure 2, and the u-shapes illustrates in Figures 3 and 4. The  
15 masses 14, 16 may be of the same approximate size as illustrated in Figure 2, or the masses 14, 16 may be of respectively different sizes as illustrated in Figures 3, 4 and 5.

          As described above, in the exemplary AVA 10 of the inventions, the base mass 14 and the absorber mass 16 are not rigidly connected directly to  
20 each other. Rather, the base mass 14 and the absorber mass 16 are connected by two switching elements 18, 20 that may be connected in parallel with respect to each other and between the masses 14, 16. The four elements, 14, 16, 18, and 20 complete a magnetic circuit. When the magnetic field is applied by the magnetic field source 22, the absorber mass  
25 16 is attracted towards the base mass 14.

          The switching elements 18, 20 may be composed of “smart materials” to complete the magnetic circuit with the base mass 14 and the absorber mass 16, and also to function as “springs”. The switching elements 18, 20 may be any spring-like device with state-dependent static displacement  
30 lengths, such as bistable springs, or springs with variable numbers of active



5 coils or close-wound springs. For example, the switching elements 18, 20 may be discrete, noncontinuous iron paths with passive spring(s) used. As another example, any discrete magnetically-conducting path (for example, iron threads in cloth, where no one thread runs from the absorber mass to the base mass) can be placed in parallel with a spring to induce an increased  
10 stiffness effect. The switching elements 18, 20 may “match” or be approximately the same in size and composition (or even other characteristics) as illustrated in Figures 1, 2, 3, and 4.

Alternatively, one of the switching elements 18, 20 may be different from the other in size, composition or other characteristics as illustrated in  
15 Figure 5 so long as the principles of the inventions are followed. Further, the Figures illustrate two switching elements 18, 20, but more or less switching elements may be used with compliance of the principles of the inventions. The Figures also illustrate the switching elements 18, 20 to be disposed in parallel with respect to each other, but that does not have to be  
20 the case so long as the principles of the inventions are followed.

In the exemplary AVA 10, the switching elements 18, 20 are made of a magnetorheological (MR) elastomer, which may be any elastomeric substance mixed with magnetically-conducting particles prior to curing. After the cure, the magnetically-conducting particles are no longer able to  
25 move freely as if they were in a fluid suspension. The MR elastomer may not be structurally rigid, nor may the elastomeric substance be magnetically-conducting. Examples of elastomeric substances include silicone gels, and natural or synthetic rubbers. The magnetically-conducting parties used with the elastomeric substance in the MR elastomer should be sufficiently small  
30 so as not to run the length (between the masses 14, 16) of the MR

5 elastomer's body. Examples of magnetically-conducting materials include iron micropowder, and low-carbon steel power or shavings.

The MR elastomer of the exemplary embodiment uses a two-part silicone gel known as GE Silicone RTV6186. The silicone gel is embedded with iron particles that become aligned in chains. When a magnetic flux  
10 path flows through this composite material, the magnetic forces oppose any displacement the iron particles experience away from their magnetic equilibrium point. The magnetic strength forces the composite material to statically compress. This causes the effective stiffness of the silicone to increase. Another cause of the change in stiffness is due to the magnetic  
15 poles on the masses 14, 16.

In the exemplary AVA 10, the MR elastomer was prepared by mixing a desired percent iron to part B of a two-part silicone mixture. As noted, the silicone was GE Silicone RTV6186, and the iron was from ISP Technologies, R 1430. An equal mass part A was added to the mixture. The  
20 silicone was mixed for ten minutes on a hot plate heated to 50 degrees Celsius. The silicone mixture was then cured for thirty minutes at an elevated temperature while a large coil had 4.5 A current running through it, magnetically saturating the iron particles and forcing them to align in chains. The silicone produced was cylindrical. Once cured, the silicone was cut in  
25 half length-wise and each half was secured to the masses 14, 16 using Loctite 454 epoxy.

Also in the exemplary AVA 10, and with respect to the percent of iron in the silicone mixture, a 5:1 maximum to minimum frequency ratio could be achieved by using the 30-35% iron by volume range with the best iron

5 percent to be around 35 % iron fraction by volume. Note: the design is iron-  
percentage dependent and “best” iron fraction may vary.

In some cases, the absorber mass 16 may be too heavy for a silicone  
mixture in the switching elements 18, 20 to support. Talc powder may be  
added to strengthen the silicone when not enough iron powder could  
10 otherwise be present, i.e., for small percentages of iron. Otherwise, the iron  
powder provides strengthening for the silicone and a means for magnetic  
flux to pass through what would otherwise be effectively an air gap.

An MR elastomer of length 1 whose stiffness change is directly  
proportional to the magnetic flux that runs through it should have a  
15 maximum flux change for the least amount of power input. Therefore, two  
MR elastomers can be placed in parallel as seen in the exemplary AVA 10.

Figure 1 illustrates a magnetic field source 22 for inducing and/or  
changing the magnetic flux in the magnetic circuit of the exemplary AVA  
10. The exemplary embodiment includes a coil of current-bearing wire (also  
20 referred to as magnet wire or a solenoid) as the magnetic field source 22 as  
illustrated in Figures 2 and 3. The coil of current-bearing wire (and any  
other magnetic field source 22) may be disposed about the base mass 14 as  
illustrated in Figure 2 or about the absorber mass 16 as illustrated in Figure  
3. A design constraint on the magnetic field source 22 is that its placement  
25 should not affect the motion of the switching elements 18, 20.

Changing the magnetic flux, as noted above, changes the frequency of  
vibration absorption by the AVA 10. When the magnetic field is applied,  
the MR elastomer of the switching elements 18, 20 of the exemplary AVA  
10 is saturated. In other words, when current flows through the coils of the  
30 exemplary magnetic field source 22, the exemplary AVA 10 experiences a

5 relatively large stiffness increase. The large stiffness increase is generated because the elastomer motion is not limited by the geometric constraints.

It should be emphasized that the above-described embodiments of the present invention are merely possible examples of implementations, merely set forth for a clear understanding of the principles of the invention. Many  
10 variations and modifications may be made to the above-described embodiments of the invention without departing substantially from the principles of the invention. All such modifications and variations are intended to be included herein within the scope of this disclosure and protected by the following claims.